

# Effects of the Perhydropolysilazane Spin-on-Dielectric Passivation Buffers on the Reliability of AlGaIn/GaN HEMTs

Mustazar Iqbal, Pil-Seok Ko, and Sam-Dong Kim

**Abstract**—AlGaIn/GaN high electron mobility transistors (HEMTs) are fabricated using a perhydropolysilazane spin-on-dielectric (SOD) buffered structure with the  $\text{Si}_3\text{N}_4$  passivation, and the effects of SOD-buffers on high electric field degradation and high temperature stability are investigated. After the high-electric field stresses (high power-state and off-state) applied to the HEMTs, we observe significantly enhanced high-electric field reliability in terms of the DC current collapse (20 and 9 % for high-power state and off-state stress, respectively) from the SOD-buffered structure compared to that of the conventional passivation structure (44 and 18 % for each case). The SOD-buffered structure also shows an improved high temperature stability producing a lower saturation drain current reduction of 49 % than that of the conventional structure (60 %) at 300 °C. It is proposed that the reliability enhancement of SOD-buffered structure is due to the reduction in surface state density at the passivation interface and the suppressed electron trapping.

**Index Terms**—Current collapse, high-temperature, reliability, SOD-buffer passivation.

## I. INTRODUCTION

AlGaIn/GaN high-electron mobility transistors (HEMTs) are recently highlighted as a key device candidate for high frequency, high power, and high temperature applications due to their strengths in material properties such as high breakdown voltage and wide band-gap. A great deal of research progress has been reported in AlGaIn/GaN HEMTs, especially, in high power applications [1] showing a significant development in the direction of product commercialization as well; however, they still need to overcome obstructions on the road by revealing themselves the reliable operation at high-electric field and high temperature stability [2].

GaN HEMTs are able to work at very high drain to source voltage because of their high breakdown voltages. However, due to the presence of high-electric field, the charged carriers can gain very high energy, consequently, activates the hot-electron phenomena (electron trapping in the surface) [3].

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One of the possible solutions to overcome this problem is to provide surface passivation. Passivation of the surface can improve the high-electric field reliability of GaN HEMT due to the minimized electron trappings at the surface states which depletes two-dimensional electron gas (2DEG) in the channel and induces the surface leakage current [4].

GaN high-power microwave devices also must function properly at high temperature without external cooling. In spite of their high band-gap property, they still suffer the drain current density reduction at elevated temperatures. For example, a 50 % decrease in saturation drain current density was reported from the AlGaIn/GaN HEMTs on SiC [2] with increasing temperature equal to 250 °C. The drain current density reduction of ~60 % was also reported in conventional GaN channel HEMTs at 300 °C [5].

No extensive study has been reported to date on DC characteristics of the GaN HEMTs with SOD-buffered passivation structures at elevated temperature. In this work, we examine the effect of the thin SOD-buffer layer spun on the HEMT on hot-electron reliability and high temperature stability compared to the conventional PECVD  $\text{Si}_3\text{N}_4$  passivation structure. A comprehensive DC characterization for the HEMTs of two different passivation structures is performed before and after the high power stress and temperature elevation up to 300 °C.

## II. EXPERIMENTS

Epitaxial structures used in this study (AlGaIn/GaN HEMTs) were grown on Si (111) substrates by metal organic chemical vapor deposition. As shown in Fig. 1, the structure consists of buffer layers, unintentionally doped channel (3000-4000 nm), and AlGaIn barrier layer with an Al composition of 25 % from the bottom. At top of the AlGaIn layer, a GaN cap layer (1.25 nm) was finally grown to decrease the gate leakage current and ohmic contact resistance.

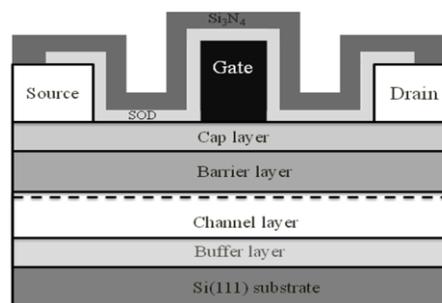


Fig. 1. Cross-section view of the HEMT with SOD-buffered passivation.

Cross sectional schematic of the SOD-buffered passivation structure is also shown in Fig. 1. To fabricate the HEMTs, mesa etching was first performed in order to isolate the active device areas by removing the 200 nm thickness of the neighboring areas in a reactive ion etching system using  $\text{BCl}_3$  plus  $\text{Cl}_2$  gases. The source and drain contacts were formed using electron-beam evaporation Ti/Al/Ni/Au layers (30/180/40/150 nm) annealing at 900 °C for 35 s in  $\text{N}_2$  ambient. The Ni/Au (40/100 nm) Schottky gate electrodes were patterned by optical lithography with a gate-length of 2  $\mu\text{m}$ , a gate width of 100  $\mu\text{m}$ , and an extension of 2  $\mu\text{m}$  from the source/drain to the central gate. In the case of buffered passivation structure, the  $\text{SiO}_x$  SOD-buffered films were coated after the gate metallization to protect the surface from plasma damage during the plasma-enhanced chemical vapor deposition  $\text{Si}_3\text{N}_4$  deposition. For the SOD layers, a dibutyl ether solution of perhydropolysilazane (PHPS) was used as a silica source (1.0 wt%, UP chemical, Ceramable™) followed by prebake and curing at 400 °C using hot-plate for 3 min, and the final thickness was about 50 nm. Fig. 2 is showing the planner view of SOD-buffer fabricated AlGaIn/GaN EHMT. The additional information for thin film characteristics of the coated PHPS  $\text{SiO}_x$  are described in our earlier report [6]. Finally,  $\text{Si}_3\text{N}_4$  passivation layer with a thickness of 100 nm deposited at a RF power of 1 kW, and the pad-opening was finally performed.

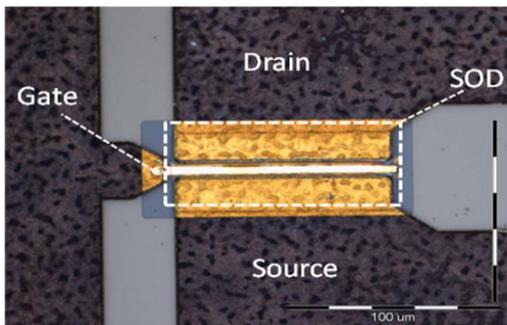


Fig. 2. Planner view of SOD-buffer AlGaIn/GaN HEMT.

### III. OFF-STATE AND HIGH POWER STATES

High electric field stress experiments were performed on the AlGaIn/GaN HEMTs of SOD-buffered and conventional  $\text{Si}_3\text{N}_4$  passivation structure. During the high power operation, both the hot-electron damage and the thermal effect due to self-heating can play roles in device degradation. However, the channel is open in off-state operation, the self-heating does not play any role in device degradation, instead of that, high-electric field present between the drain and gate region can degrade the device. With the aim to separate these possible source of degradation in high-electric field stress, we carry out two kinds of stress schemes of high-power step-stress (at  $V_{ds} = 0$  to 40 V in steps of 5 V per 30 min and  $V_{gs} = 1$  V) and off-state step-stress (at  $V_{ds} = 0$  to 40 V in steps of 5 V per 30 min and  $V_{gs} = -6$  V) with a computer controlled test arrangement connected to Agilent source measure unit (SMU) B2902A at room temperature in air. Stress experiments were carried out on 20 samples (10 samples for high-power state step-stress and 10 samples for off-state step-stress) in total.

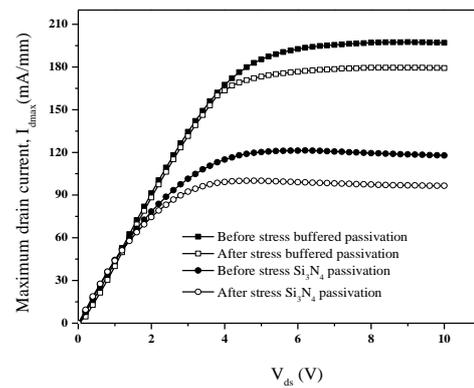


Fig. 3.  $I_{dmax}$  versus  $V_{ds}$  of the AlGaIn/GaN HFMTs with SOD-buffered and conventional  $\text{Si}_3\text{N}_4$  passivations before and after the off-state step-stress. Devices were stressed at  $V_{ds} = 5$  to 40 V with a step of 5 V per 30 min and at  $V_{gs} = -6$  V.

Fig. 3 illustrates the impact of 240-min off-state step-stress on  $I_{dmax}$  of two different passivation structures (SOD-buffered and  $\text{Si}_3\text{N}_4$  passivations) for the AlGaIn/GaN HEMTs. As shown in the measurements, the average  $I_{dmax}$  drop is more severe in the conventional  $\text{Si}_3\text{N}_4$  passivation structure than that of the SOD-buffered structure; for example, the reductions in  $I_{dmax}$  (at  $V_{ds} = 10$  V and  $V_{gs} = 1$  V) produced by the off-state step-stresses were 18 and 9 % for the conventional and buffered structure, respectively. On the other hand, there was negligible threshold voltage ( $V_{th}$ ) shift in both structures after the off-state step-stress.

Fig. 4 shows the normalized average  $I_{dmax}$  values measured before and after the high power-state step-stresses for 240 min in total. Degradation ratio in average  $I_{dmax}$  of the conventional passivation structure (~44 %) was almost two times greater than that of the buffered structure (~20 %). There were small positive shifts of the  $V_{th}$  in both cases, however they were negligible too. Degradations in  $I_{dmax}$  after the high-power state step-stress were higher those measured after the off-state step stress in both cases.

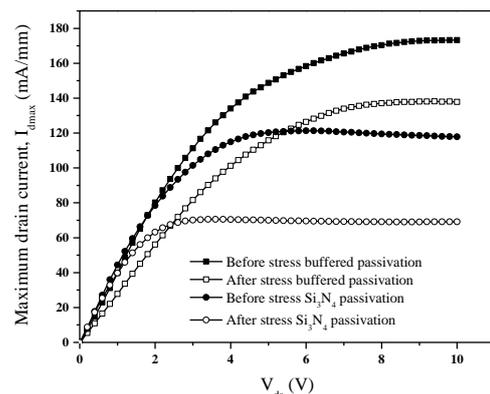


Fig. 4.  $I_{dmax}$  versus  $V_{ds}$  of the AlGaIn/GaN HFMTs with SOD-buffered and conventional  $\text{Si}_3\text{N}_4$  passivations before and after the high-power state step-stress. Devices were stressed at  $V_{ds} = 5$  to 40 V with a step of 5 V per 30 min and at  $V_{gs} = 1$  V.

Enhancement in high-electric field reliability of SOD-buffered structure devices can be attributed to the minimization in surface state density and trap centers. The electron trapping centers are attributed to the material imperfections or damaged layer produced by the device process; for example, plasma and thermal damage can

produce nitrogen vacancies at the AlGaIn layer surface [7] accounting for the current collapse. Even though the role of hot electrons in activating and/or converting the pre-existing carrier traps is not fully understood in hot carrier stress regime, our results propose that, during the stress stage, hot electrons from the channel can gain sufficient energy to overcome the energy barrier existing in the extrinsic region of the barrier/cap region and get trapped at the interface of the passivation. This leads to the change in electrostatics such that they deplete channel carrier concentration in the extrinsic drain, resulting in DC current collapse in the operation mode. Therefore, it can be postulated that our SOD-buffered passivation structure which is relatively free from plasma-damage provides a much lower density of trap centers than the conventional passivation structure; therefore, it can show a significant enhancement in DC reliability by minimizing the deleterious imperfections at the passivation interface known to be the most prominent trap centers.

#### IV. TEMPERATURE STABILITY

The AlGaIn/GaN HEMT are anticipated for high temperature application due to its high band-gap energy. But as the temperature increased of AlGaIn/GaN HEMT, its mobility and saturation velocity decreased. In order to examine the high temperature parameters stability,  $I_{dss}$ ,  $g_{m,max}$  and  $V_{th}$  of for the AlGaIn/GaN HEMTs of two different passivation structures were measured in a temperature range of 25-300 °C, and 10 samples in total were measured for this experiment (5 from the SOD-buffered structure and 5 from the conventional passivation structure).

Fig. 5 shows the effect of temperature on  $I_{dss}$  (measured at  $V_{ds} = 10$  V and  $V_{gs} = 0$  V) normalized based on the reference values measured at 25 °C for two different passivation structures AlGaIn/GaN HEMTs. Typical trends of current reduction with the temperature increase were observed in both structures. However, it is also obviously shown that the amount of current degradation of the buffered passivation structure is only ~49 % ( $\sigma = 1.5$ ) and much lower than that of the conventional passivation structure (~60 %) at 300 °C.

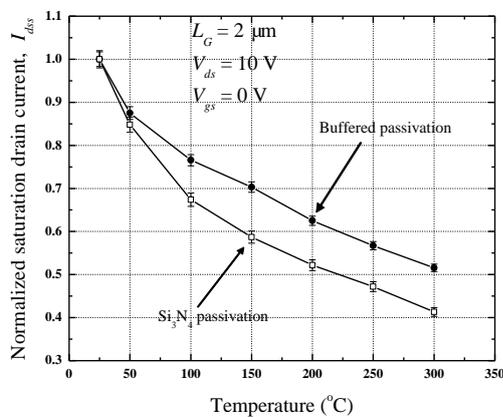


Fig. 5. Normalized saturation drain current as a function of temperature measured from the AlGaIn/GaN HFMTs of SOD-buffered and conventional  $Si_3N_4$  passivation structures.

Shown in Fig. 6 are the average  $g_{m,max}$  normalized based on the reference values measured at 25 °C for two different

passivation structures. The SOD-buffered structure also showed significantly enhanced high temperature stability in terms of  $g_{m,max}$  reduction (~34 and ~44 % for the buffered and conventional passivation structure, respectively) at 300 °C. As shown in Fig. 7, the  $V_{th}$  shifts after the temperature elevation up to 300 °C were +0.25 and +0.28 V for the buffered and conventional passivation structure, respectively.

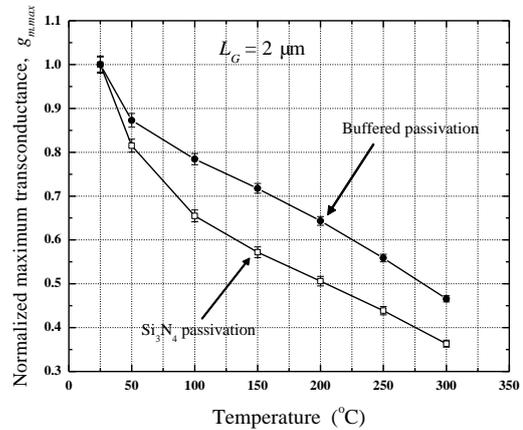


Fig. 6. Normalized maximum transconductance as a function of temperature measured from the AlGaIn/GaN HFMTs of SOD-buffered and conventional  $Si_3N_4$  passivation structures.

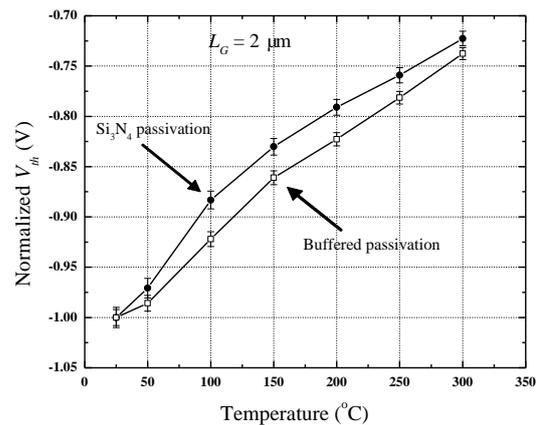


Fig. 7. Normalized threshold voltage as a function of temperature measured from the AlGaIn/GaN HFMTs of SOD-buffered and conventional  $Si_3N_4$  passivation structures.

#### V. CONCLUSIONS

In summary, a novel AlGaIn-GaN HEMT structure of high temperature stability and high electric field reliability was successfully demonstrated by employing the  $SiO_x$  SOD-buffered passivation. After the off-state and high power states stresses, it was shown that the SOD-buffered HEMTs showed significantly smaller reduction in  $I_{dmax}$  compared to that of the conventional passivation structure. We also observed that the key device parameters of  $I_{dss}$ ,  $g_{m,max}$  and  $V_{th}$  measured from the  $SiO_x$  SOD-buffered passivation structure were more stable against the temperature elevation up to 300 °C than those of the conventional passivation structure. We propose that this enhancement was due to a much lower density of trap centers at the SOD-buffered passivation structure than that of the conventional passivation structure.

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